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SOV/180-59-6-10/31

Irreversible Temper Brittleness in Constructional Steels

associated with the process of decomposition of martensite, it is not possible completely to prevent the development of this weakness. However, the data published in the literature (Refs 6, 14, 28) and the results of the present investigation indicate several ways of minimizing the harmful effect of tempering on the mechanical properties of steels. This can be achieved by 1) lowering the threshold temperature of cold-shortness of steels tempered at low temperatures (by grain-refining and lowering the content of solid and gaseous impurities); 2) shifting the critical tempering temperature range towards higher temperatures by means of alloying additions which inhibit the decomposition of martensite; and 3) ensuring more uniform decomposition of martensite.

There are 7 figures and 28 references, of which 19 are Soviet and 9 English.

Card
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SUBMITTED: August 6, 1959

18(0),24(2)

Sarrak, V. I.

SOV/53-67-2-4/7

AUTHOR:

The Brittle Breaking of Metals (Khrupkoye razruskeniye metallov)

TITLE:

Uspekhi-fizicheskikh nauk, 1959, Vol 67, Nr 2, pp 339-361 (USSR)

PERIODICAL:

ABSTRACT: The present paper gives a survey of theoretical and experimental investigations of problems concerning the brittle destruction of metals. By this one understands a breaking or tearing of metal, by which, without any previous noticeable plastic deformation, two new surfaces are created (plastic destruction is, however, preceded by a considerable plastic deformation). In his introduction the author shows that the theoretical calculation of the strength of metals according to the formula

$$\sigma_{\text{theor}} = \sqrt{(E \gamma/a)},$$
 where E denotes Young's modulus, γ the surface energy connected with the forming of two new surfaces, and a the atomic lattice constant, yields a value that is much too high. Chapter 2 deals with the theory by Griffith (Ref 1), which gives the formula
$$\sigma = \sqrt{(2E \gamma/\pi c)},$$
 and the formula by Orovyan (Ref 4) of

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The Brittle Breaking of Metals

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$\sigma = \sqrt{(2E_p/\pi c)}$, where the plastic deformation of the surface layer is already taken into account. Chapter 3 in detail deals with the dislocation theory of destruction, and chapter 4 deals with the temperature course of the yield point. (Figures 6-9 show respective diagrams). In the following chapter the part played by impurities of the lattice is investigated, and chapter 6 deals with the structure of steel and its tendency towards brittle breaking, and chapter 7 deals with intergranular destruction. The last part of the paper discusses the spreading of cracks according to the deformation- and dislocation theories. Figure 12 shows the increase of stress in a brittle crack in soft steel in dependence on temperature; the diagram shows, in this case at 10°C, the characteristic and practically vertical increase of transversal stress. The following Soviet authors are mentioned: A. V. Stepanov, Ya. I. Frenkel', Ya. M. Potak, B. S. Kasatkin, S. S. Shurakov, S. Tsobkallo, F. F. Vittman, G. V. Uzhik, N. N. Davidenkov, T. N. Chuchman, V. I. Kostenets, S. I. Sakhin, P. O. Pashkov, V. A. Bratukhina, Ye. M. Shevandin, L. G. Orlov, I. M. Utevskiy. There are 12 figures and 78 references, 19 of which are Soviet.

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SOV/20-127-2-20/70

AUTHORS: Sarrak, V. I., Entin, R. I.

TITLE: On Relaxation-processes During the Recrystallization and the Deep Annealing of Hardened Steel

PERIODICAL: Doklady Akademii nauk SSSR, 1959, Vol 127, Nr 2, pp 306-309
(USSR)

ABSTRACT: Hardened samples of three steel alloys were annealed at different temperatures for one hour, and changes in the limit of resistance were then investigated. The results of these tests are given in table 1. The effect of annealing of hardened samples on the width of the X-ray interference bands is also investigated. Relevant data are given in table 2. From the fact that the width of interference bands decreases but slightly even when samples are subjected to higher annealing, it is concluded that the bands are not connected with the breaking down of the martensite structure. However, the decrease in width of the interference bands is explained by the existence of elastic deformations in the micro-regions (tensions of the second kind). As may be seen from the diagram (Fig 1) the resistance at 20°C reaches a limit 5 to 6 hours after hardening. The same is valid

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On Relaxation-processes During the Recreation and the SOV/20-127-2-20/70
Deep Annealing of Hardened Steel

for internal friction. Further, changes in the internal friction dependent on annealing were examined by determining the free torsional vibrations. Results are listed in a diagram (Fig 2). These experiments were carried out at the Kafedra fiziki Moskovskogo instituta stali RKF-MIS (Chair of Physics in the Moscow Institute for Steel RKF-MIS). A decrease in the height of the peaks at 200°C was noted regardless of the annealing method. This observation is brought into connection with the breaking down of the martensite and with relaxation processes. Finally the dislocation-theory is discussed and it is stated that the local tensions are proportional to the accumulation of dislocations. Furthermore, studies are made of the relaxation time after deformation or after martensite transformation, and of the influence of the diffusion of atoms

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On Relaxation-processes During the Recrystallization and the SOV/20-127-2-20/70
Deep Annealing of Hardened Steel

between 120 and 280°C on internal friction. There are 2 figures,
2 tables, and 12 references, 8 of which are Soviet.

ASSOCIATION: Institut metallofiziki Tsentral'nogo nauchno-issledovatel'skogo
instituta chernoy metallurgii
(Institute for the Physics of Metals of the Central Scientific
Research Institute for Iron-metallurgy)

PRESENTED: March 30, 1959, by G. V. Kurdyumov, Academician

SUBMITTED: March 21, 1959

Inst Metal Studies & Physics of Metals,
Cent. Inst. for Iron Metallurgy,

Card 3/3

SARRAK, V. I. Cand Tech Sci -- "Friability of steel in low-temperature tempering."
Mos, 1960 (Min of Higher and Secondary Specialized Education RSFSR. Mos Order
of Labor Red Banner Inst of Steel im I. V. Stalin). (KL, 1-61, 196)

83995

S/129/60/000/010/003/009
E193/E483

18.8900 2308
1045
1413
AUTHORS: Sarrak, V.I., Engineer and R.I. Entin, Doctor of
Technical Sciences, Professor

TITLE: Reversible Temper Brittleness

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov,
1960, No. 10, pp. 14-19

TEXT: The main results of the investigation, described in the present paper, are reproduced graphically in Fig. 7, where the critical temperature of cold-shortness of steel 20ХГ(20KhG) is plotted against tempering temperature for specimens of steel (1) quenched in oil, (2) subjected to special heat treatment leading to precipitation of ferrite at the grain boundaries, (3) remelted in vacuum, (4) heat-treated, (5) containing an addition of 0.3% Al, and (6) containing an addition of 0.002% B. Analysis of these results, correlated with the findings of other workers, led the present authors to the following conclusions:

The main cause of reversible temper brittleness is the specific character of decomposition of martensite at the grain boundaries, where the transformation often begins earlier and proceeds at a rate faster than in the interior of the grains. Tempering at low

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E193/E483

Reversible Temper Brittleness

and moderately high temperatures brings about (at a certain stage of the process) almost complete decomposition of martensite at the grain boundaries with the interior of the grains still constituting a super-saturated solid solution. The heterogeneous structure, formed in this way and containing domains of solid solution with different carbon contents, is the principal cause of the increased tendency of steel to fail in a brittle manner. When steel in this condition is stressed, the solid solution regions, characterized by low yield point, are subjected to a system of tri-axial stresses, in which case the ratio of the normal to tangential stress increases and the critical temperature of the cold-shortness is raised. Tempering, carried out at relatively high temperatures, does not cause cold-shortness since, under these conditions, no concentration gradient is formed in the solid solution. Another factor which promotes the development of reversible temper brittleness is the decrease in the free surface energy of the grains. The probability of intercrystalline fracture decreases with increasing magnitude of the difference $\gamma_n - \gamma_g$, where γ_n is the free surface energy of the grains and γ_g is the excess

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E193/E483**Reversible Temper Brittleness**

grain-boundary energy due to heavily distorted crystal lattice in these regions. Normally this difference is large but it decreases considerably in the presence of a decomposed solid solution formed at the grain boundaries of martensite, which leads to intercrystalline fracture as a result of the onset of reversible temper brittleness. It is possible that the beneficial effect of the introduction of small additions of aluminium or boron, thermal treatment, and vacuum melting on the tendency of steel to develop reversible temper brittleness is associated with the effect of these factors on the surface energy of the grains in decomposed martensite. Thus, although it is not possible to prevent the onset of irreversible temper brittleness, the critical tempering temperature can be raised by addition of elements which retard the second stage of decomposition of martensite (silicon, tungsten), and the temperature at which the tempered steel exhibits its brittle characteristics can be depressed by the application of vacuum melting, thermal and mechanical treatment and /or introduction of small additions of aluminium or boron.

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E193/E483

Reversible Temper Brittleness

There are 7 figures and 16 references: 9 Soviet, 5 English,
1 German and 1 French.

ASSOCIATION TsNIIChM

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TRANSLATION

S/180/61/000/001/008/015
E073/E535AUTHORS: Sarrak, V. I. and Entin, R. I. (Moscow)TITLE: Brittleness of Steel in Conjunction with Secondary Hardness

PERIODICAL: Izvestiya Akademii nauk SSSR, Otdeleniye tekhnicheskikh nauk, Metallurgiya i toplivo, 1961, No.1, pp.117-118

TEXT: During tempering of steels alloyed with vanadium, ²⁷ molybdenum and tungsten, an increase in hardness occurs in the temperature range 500 to 600°C, which is associated with the formation of disperse carbides of these elements. The authors of this paper investigated the tendency to brittleness of such steels in conjunction with the process of decomposition of the solid solution of carbon in the α-phase. The investigations were made for the steels 10T, 35T, 20C2Γ3+2X (20S2G3N2KhF), 30C2Γ3+1 (30S2G3N2F), 35S2Γ3+2 (35S2G3N2F), 40C2Γ3+1 (40S2G3N2F). The steel 10T was quenched from 1350°C, the remainder were quenched from 1100°C. The hardness R_C , impact strength a_k , kgm/cm^2 , width of the X-ray interference lines B , mrad, and the coercive force H_C , Oe, were measured. Fig.1; the top graph relates to the

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steel 10T (0.1% C, 0.5% Ti) for which the impact strength was determined at +120°C, the bottom graph relates to the steel 20S2G3N2KhF (0.21% C, 2.07% Si, 3.02% Mn, 1.85% Cr, 1.83% Ni, 1.57% V). For the steels 10T and 35T the hardness decreased somewhat before reaching a maximum; for the other steels an increase in hardness was observed from 400°C onwards. The decrease in the impact strength occurred after the beginning of decomposition of the solid solution, which can be evaluated on the basis of the width of the X-ray interference lines. This is particularly pronounced for the steel 20S2G3N2KhF (Fig.1b), for which the temperature of the beginning of a drop in impact strength coincides with the temp. of decomposition of the solid solution. The character of the fracture of the steel in the brittle state, corresponding to maximum hardness, is intercrystalline. If the tempering temperature is increased to 650°C, the fracture will become transcrystalline. It is pointed out that development of the brittleness begins prior to reaching maximum hardness and is associated with processes of decomposition of the solid solution. It can be assumed that the development of brittleness is to some extent the consequence of a

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Brittleness of Steel in

differing degree of decomposition of the solid solution along the boundaries and inside the grain. Decomposition of the solid solution at the grain boundaries usually occurs at greater speeds than inside the grain; it can be anticipated that the maximum degree of structural nonuniformity will correspond to a maximum hardness inside the grain, which is associated with rejection of disperse carbides. Particularly at this stage the process of decomposition can be completed along the grain boundaries. Thereby, inside the grain the saturated solid solution of carbon in α -iron, which is in metastable equilibrium with disperse rejections of special carbides, will still be maintained. This is evidenced by the nature of the changes in the widths of the interference lines of the α -phase at tempering temperatures of 300 to 500°C (Fig. 1b). The presence in the alloy of sections of solid solutions of differing composition with differing yield points brings about brittle failure, as was shown for instance by V. A. Pavlov and M. V. Yakutovich (Ref. 3) in the case of quenched steel with a ferrite network along the grain boundaries. Failure in this case will occur along the sections of the decomposed solid solution with

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Brittleness of Steel in

a lower yield point which are distributed along the grain boundaries. A further increase of the tempering temperature leads to full decomposition of the solid solution inside the grain and elimination of the structural nonuniformities of the steel. The nature of the failure changes: fractures along the grain boundaries will cease. The impact strength of the steel can increase considerably (Fig.1a), although in some cases it will remain unchanged in spite of the considerable drop in hardness (Fig.1b). It cannot be ruled out that this phenomenon in the steel 20S2G3N2KhF is associated with the difficulty of the process of coagulation of the disperse carbides due to alloying of the steel with silicon, chromium and vanadium. Consequently, the impact strength may not increase, although the hardness of the steel will drop as a result of decomposition of the solid solution of carbon in the α -iron. Obviously, for increasing the impact strength of this steel high temperature tempering is required, which leads to coagulation of the disperse special carbides. The brittleness associated with failure along the grain boundaries is obviously a phenomenon which is associated with decomposition of solid solutions if at a certain stage the degree of

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Brittleness of Steel in

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decomposition along the grain boundaries differs from that inside the grains. Such brittleness was detected by A. Geisler and F. Keller (Ref.4) in alloys of aluminium with magnesium and silicon and by A. Guy, C. Barret and R. Mehl (Ref.5) in beryllium bronze and by A. Kramer and W. Baldwin (Ref.6) in stainless chromium-nickel austenitic steel. The irreversible temper brittleness of constructional steels is also associated with differing degrees of decomposition of the solid solution of carbon in the α -iron along the boundaries and inside the grain (Ref.7). There are 2 figures and 7 references: 3 Soviet and 4 non-Soviet.

(Note: This is a complete translation)

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S/717/62/000/007/003/010
D207/D301

Brittleness of steel during tempering ...

led up and cracks were initiated. The high internal friction immediately after quenching was due to motion of dislocations. Relaxation at room temperature and tempering at 100 or 200°C reduced brittleness and internal friction by gradual relieving of internal stresses and dispersal of dislocations. In a certain range of temperatures, lying between 200 and 500°C for different steels, tempering increased brittleness because of selective precipitation, at grain boundaries, of the solid solution of carbon in α -iron. This produced a non-uniform distribution of carbon which favored cracking along grain boundaries. Tempering at still higher temperatures produced more intense precipitation of carbon, but the distribution of the precipitate became more uniform and once again brittleness decreased. Acknowledgment is made to A.I. P'yanov, Student of the Khar'kovskiy politekhnicheskiy institut im. V.I. Lenina (Khar'kov Polytechnical Institute im. V.I. Lenin) who helped in some experiments. There are 14 figures and 34 references: 17 Soviet-bloc and 17 non-Soviet-bloc. The 4 most recent references to the English-language publications read as follows: H. King and S. Glover, J. Iron and Steel Inst., 193, 123, 1959; C. Beaulien, A. Dube and G. Setendre, Trans. Met. Soc. AIME, 218, 3, 1960; R. Decker,

Card 2/3

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fittleness of steel during tempering ... D207/D301

and I. Freeman, Trans. Met. Soc. AIME, 218, 277, 1960; A. Kramer, and
W. Baldwin, Trans. ASM, 50, 803, 1958.

Card 3/3

S/129/63/000/004/001/014
A004/A127

AUTHORS: Sarrak, V.I., Entin, R.I.

TITLE: Austenite hardening during thermomechanical treatment of steel

PERIODICAL: Metallovedeniye i termicheskaya obrabotka metallov, no. 4,
1963, 2 - 4

TEXT: The steel grades 45X3H8C (45Kh3N8S) - 0.45% C, 2.68% Cr,
8.35% Ni and 1.54% Si - and 40XH3M (40KhN3M) - 0.4% C, 1.76% Cr, 2.89% Ni
and 0.72% Mo - were investigated to study the relation between the degree
of austenite hardening and the strength of steel after thermomechanical
treatment. The strength of hardened steel is determined by the level of
strength of the deformed austenite and does not depend on the temperature
at which the given degree of strength was obtained. If the austenite de-
formation temperature is reduced the coefficient of its hardening increases.
The lower the deformation temperature the more considerable is the harden-
ing of steel obtained at a lower degree of deformation. To obtain an
identical hardening of steel at higher temperature, a high degree of deform-
ation is required. It cannot be excluded that in the latter case, at the

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Austenite hardening during ...

S/129/63/000/004/001/014
A004/A127

same degree of strength after thermomechanical treatment, the steel will possess a higher ductility. There are 4 figures.

ASSOCIATION: TeNIIChM

Card 2/2

L 21731-65 EWT(m)/EWA(d)/T/EWP(t)/EWP(k)/EWP(b) Pr-1 AFWL/SSD/ASD(f)-3/
ASD(m)-3 JD/HW
ACCESSION NR: AP4043921 S/0279/64/000/004/0127/0130

13

AUTHOR: Suvorova, S.O. (Moscow); Sarrak, V.I. (Moscow); Entin, R.I. (Moscow)

TITLE: Investigation of the strain aging of iron by the internal-friction method

SOURCE: AN SSSR. Izv. Metallurgiya i gornoye delo, no. 4, 1964, 127-130

TOPIC TAGS: strain aging, iron, titanium, hydrogen annealing, internal friction, strain amplitude, dislocation, interstitial atom

ABSTRACT: The authors investigated strain aging by a method that made a study of the correlation between dislocations and interstitial atoms possible. Iron specimens containing 0.03% C, 0.006% N₂ and 0.33% Ti were annealed for 60 minutes at 950C, furnace cooled and water quenched from 720C. Aging in a thermostat at 60C was followed by torsion tests. The authors found that strain aging had been brought about by the interaction of carbon and nitrogen atoms. The assessment of the characteristics of internal friction and, primarily of its amplitudinal dependence in electrolytic iron showed that dislocations were fixed

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L 217.1-35

ACCESSION NR: AP4043921

by C and N₂ atoms which formed "clouds", segregated and, finally, precipitated as the aging period was extended. The concentration of free C and N₂ atoms which were not bound to dislocations was established at 40C. The investigation of the critical strain amplitude led to the assumption that the purification of iron in hydrogen causes the amplitude to become negligible. Thus, the amplitude lies outside the range within which the authors were able to measure internal friction. Additions of Ti or hydrogen annealing greatly lowered the concentration of N₂ and C in the α -iron solid solution. This drop in concentration was reflected in the disappearance of the peak of the temperature curve at 40C. Subsequently strain aging and the area of yield were eliminated, so that the value of the yield point did not increase. On the other hand, holding at 60C for several hours neither affected the critical strain amplitude nor changed the concentration of C and N₂ atoms on dislocations. The authors' data coincide with earlier investigations on the nature of strain aging in iron. Orig. art. has 4 figures.

ASSOCIATION: None

SUBMITTED: 16Nov63

SUB CODE: MM

Card 2/2

ENCL: 00

NO REF SOV: 013 OTHER: 003

L 45182-65 EWT(m)/EWP(w)/EPF(n)-2/EWA(d)/T/EWP(t)/EWP(k)/EWP(z)/EWP(b)/EWA(c)
PF-1 P-4 ICP(1) MJW/JD/HW/JG

ACCESSION NR: AT5011202

UR/2717/64/000/008/0044/0057

AUTHOR: Kogan, L. I.; Sarrak, V. I.; Entin, R. I.

53
P+1

TITLE: Thermomechanical treatment of steel

Dnepropetrovsk, Institut metallovedeniya i fiziki metallov.
Metallovedeniya i fiziki metallov, no. 8, 1964, 44-57

KEY WORDS: thermomechanical treatment, thermomechanical property, steel, steel hardening, steel microstructure, austenite, austenitic steel, austenitic transformation, carbon, alloying, vacuum melting, metal deformation, stress load, yield strength, metal ductility, molybdenum containing alloy, tungsten containing alloy, molybdenum containing alloy, vanadium containing alloy, nickel containing alloy

ABSTRACT: The steels investigated were 40KhN5S, 42KhN5SMF, 44Kh5MF, 30Kh1, 45Kh3N8SM, 40KhN3M, 05Kh9N3, 11Kh9N3, 24Kh9N3, 30KhN5S, 35KhN5S, and 35KhN5G. Their compositions varied within the limits of 0.35-0.41 chromium, 0.12-1.00 silicon, 0.30-0.80 manganese, 1.65-1.93 chromium, 2.89-8.35 nickel, 0.48-2.93 molybdenum, and 0.25-0.82 vanadium. The mechanical properties sigma_b kg/mm²,

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ACCESSION NR: AT5011202

delta %, psi %, and HRC were determined under different thermomechanical treatment conditions. The influence of stress and deformation on the kinetics of austenite transformation was investigated at 300 and 525°C. A load was applied at a rate of 0.6 mm/min up to the desired stress which was then held constant at ± 1 kg/mm². For steel 10KhN8S the yield point of precooled austenite was 15-20 kg/mm² at 20°C and 35-37 kg/mm² at 300°C. The reasons for hardening with thermomechanical treatment were investigated. This investigation covered the hardening of austenite during heat and mechanical treatment, the microstructure of steels after thermomechanical treatment, and X-ray investigation of the fine structure of the steels after treatment. Based on the experimental data, the following conclusions were reached: 1) carbon content should not exceed 0.40-0.45% since further increase leads to considerable lowering of impact resistance and ductility properties and makes deformation of the austenite difficult; 2) alloying should assure high stability of austenite since in the opposite case the effect of deformation on the kinetics of the transformation can bring about formation of non-martensite transformation products; 3) alloying with silicon is expedient to prevent decomposition of martensite and a shift of the interval of

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L 45182-65

ACCESSION NR: AT5011202

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irreversible temper brittleness to higher temperatures; 4) for strength retention at high temperatures it is expedient to alloy with elements which bring about secondary hardness (tungsten, molybdenum, and tantalum); and 5) vacuum melting of pure starting materials permits attainment of ductility. Orig. art. has: 13 figures and tables.

ASSOCIATION: None.

SUBMITTED: 00

ENCL: 00

SUB CODE: MM

NR REF Sov: 016

OTHER: 009

b7c
Card 3/3

SARRAK, V.I.; SUVOROVA, S.O.; ENTIN, R.I.

Studying the phenomenon of the deformation aging of iron. Probl. metal-loved. i fiz. met. no.8, 125-143 '64. (MIRA 18:7)

SUVOROVA, S.O.; SARAK, V.I.; ENTIN, R.I.

Investigating the deformation aging of commercial-grade iron. Fiz. met.
i metalloved. 17 no.1:105-111 Ja '64. (MIRA 17:2)

1. Institut metallofiziki TSentral'nogo nauchno-issledovatel'skogo
instituta chernoy metallurgii im. Bardina.

I 36624-65 EWT(m)/EMP(w)/EWA(d)/T/EMP(t)/EMP(l)/EMP(b)/EWA(e) PR-4/red 1 P(c)
ACCESSION NR: AP5002350 MJW/JD/HW S/0126/64/018/006/0915/0920

AUTHOR: Spektor, Ya. I.; Sarrak, V. I.; Entin, R. I.

b1
b2
b3

TITLE: Tendency toward brittle fracture and the fine structure of steel

SOURCE: Fizika metallov i metallovedeniye, v. 18, no. 6, 1964, 915-920

TOPIC TAGS: brittle fracture, steel, OKh7 steel, ON4 steel, 30KhGSNA steel,
fine structure, impact strength, ductile fracture, cold brittleness, grain boundary crystal structure, hardening plastic deformation, ferrite grain size

ABSTRACT: The effect of changes in the fine structure of steel developed by plastic deformation and phase hardening on its inclination toward brittle fracture was studied. The critical temperature T_{crit} (at which impact strength started to fall rapidly) was determined from impact strength-temperature curves; the impact strength a_{kmax} during ductile fracture was determined; values of type II distortion $\Delta a/a$ and the extent of the range of coherent scattering D were determined from x-ray interfreredence data on OKh7, ON4 and 30KhGSNA steels. T_{crit} was lower-

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ACCESSION NR: AP5002350

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ed as $\Delta a/a$ decreased; when the tempering temperature was raised and the growth of D increased noticeably, T_{crit} continued to fall and a_{kmax} started to increase. The greatest reduction in T_{crit} upon heating annealed and cold deformed alloys occurred at temper temperatures at which $\Delta a/a$ decreased and D increased. The threshold of cold brittleness of hardened and deformed iron alloys depends on internal stresses whose reduction leads to reduction in T_{crit} ; this process starts to develop on heating well below the temperature at which D starts to increase. Tempering at higher temperatures reduced $\Delta a/a$ and D, and T_{crit} . It was concluded that the reversible and irreversible temper brittleness of steel was associated with the conditions of the grain boundaries and not with changes in the fine crystal structure of the grain. Impact strength at temperatures above the brittleness T_{crit} is determined by the state of the ferrite matrix of the steel, but other factors such as the presence of the carbide phase, its form, dispersity and distribution must be considered. The tendency toward brittle fracture can be reduced by reduction of the ferrite grain size and by alloying, e.g., with nickel.²⁷

Orig. art. has 8 figures.

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L 36624-65

ACCESSION NR: AP5002350

ASSOCIATION: Institut metallovedeniya i fiziki metallov TsNIIChERMET im.
I. P. Bardina Zavod "Dneprospetsstal'" (Institute of Metal Science and Physics
of Metals, Central Scientific Research Institute of Ferrous Metallurgy)

SUBMITTED: 22Feb64

ENCL: 00

SUB CODE: MM

NR REF SOV: 013

OTHER: 000

Card 3/3

ACCESSION NR: AP4034537

S/0020/64/155/005/1054/1057

AUTHOR: Spektor, Ya. I.; Sarra, V. I.; Entin, R. I.

TITLE: Explanation of the effect of nickel on cold shortness of iron

SOURCE: AN SSSR. Doklady*, v. 155, no. 5, 1964, 1054-1057

TOPIC TAGS: iron cold shortness, nickel iron alloy, plastic deformation, internal friction, ductility brittleness transition

ABSTRACT: Alloying of commercial iron and construction steels with nickel considerably lowers the temperature of transition from a ductile to a brittle state in impact tests. The authors have investigated this phenomenon on iron with 0.03% C (MZh), with and without 3.4% Ni (ON4). The heat treatment was such that the grain size was the same in both materials. Impact tests were conducted in the temperature range from +100 to -196 C. Alloying lowered the brittleness temperature by about 30 C. Since the interaction between the interstitial atoms (carbon, in this case) and dislocations which cause brittleness is reflected in the amplitude dependence of internal friction; the authors determined the latter with a torsion pendulum. The critical amplitude which was found at 20 to 200C is considerably

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ACCESSION NR: AP4034537

lower in nickel iron. This shows that the interaction of dislocations with carbon are weaker, thus lowering the fixation of dislocations and favoring plastic deformation. Orig. art. has: 4 figures.

ASSOCIATION: Institut metallovedniya i fiziki metallov central'nogo nauchno - issledovatel'skogo instituta chernoy metallurgii im. I. P. Bardina (Institute for Metallurgy and Physics of Metals of the Institute for Ferrous Metallurgy).

SUBMITTED: 06Nov63

DATE ACQ: 13May64

ENCL: 00

SUB CODE: M, MM

NO REF Sov: 005

OTHER: 007

Card
1/2

SARRAK, V.I. (Moskva); SUVCROVA, S.O. (Moskva); ENTIN, R.I. (Moskva)

Effect of deformation and aging on the amplitude characteristic
of internal friction in martensite. Izv. AN SSSR. Mat. no.4:156-
158 Jl-Ag '65. (MIRA 18:8)

L 1627-66 EWT(m)/EWP(w)/T/EWP(t)/EWP(b)/EWA(c) JD

UR/0126/65/020/002/0315/0316
539.67

ACCESSION NR: AP5021947

AUTHOR: Sarrak, V. I.; Suvorova, S. O.

TITLE: Effect of tempering on the amplitude dependence of the internal friction
of martensite

SOURCE: Fizika metallov i metallovedeniye, v. 20, no. 2, 1965, 315-316

TOPIC TAGS: internal friction, tempering, martensite, solid solution, carbide phase

ABSTRACT: Following low-temperature tempering (approx. 100°C) the amplitude-independent internal friction of the martensite of 20KhG steel decreases; this may be associated with the stress-relaxation processes. (The amplitude mentioned here refers to deformation amplitude.) Tempering in the 200-400°C range, which leads to a virtually complete decomposition of the solid solution, produces an increase in both the amplitude-independent internal friction Q^{-1} and the amplitude-dependent internal friction α . This may be due to the increase in the mobility of dislocations owing to the decomposition of the solid solution. The decrease in Q^{-1} and α at tempering above 400°C is apparently to be explained by the decrease in the

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ACCESSION NR: AP5021947

dislocation density of the matrix and the coagulation of the carbide phase. Thus, the change in the characteristics of internal friction may be related to the processes of martensite decomposition and the decrease in dislocation density during tempering. A detailed elucidation of this relationship requires further investigation. Orig. art. has: 2 figures.

ASSOCIATION: Institut metallofiziki (Institute of Metal Physics); TsNIIGChERMET
im. I. P. Bardina

SUBMITTED: 07Aug64

ENCL: 00

SUB CODE: RM, ME

NO REF SOV: 004

OTHER: 000

Card 2/2 00

L 1626-66 EWT(m)/EWP(w)/T/EWP(t)/EWP(b)/EWA(c) IJP(c) JD
ACCESSION NR: AP5021948 UR/0126/65/020/002/0317/0319
546.72:539.67:539.374 4/1
4/2
4/3

AUTHOR: Beresnev, G. A.; Sarrak, V. I.

TITLE: Effect of plastic deformation on the amplitude dependence of the internal friction of iron

SOURCE: Fizika metallov i metallovedeniye, v. 20, no. 2, 1965, 317-319

TOPIC TAGS: internal friction, material deformation, amplitude, iron, crystal lattice

ABSTRACT: The effect of plastic deformation on the change in the (deformation-) amplitude-dependent internal friction Δ_h at temperatures of from 20 to -160°C in constant longitudinal magnetic fields of different intensity was investigated for commercial iron containing 0.025% C, 0.20% Si, 0.12% Mn, 0.01% S, 0.004% P, and 0.02% Al. Internal friction was measured by recording the damping of the natural torsional vibrations of 0.8 mm diameter wire specimens at a frequency of ≈ 0.8 cps. It was found that magnetoelastic scattering markedly decreases as a result of plastic deformation (curve 1, Fig. 1). This is because the deformation involves a considerable increase in the number of dislocations, whose stress fields are obsta-

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ACCESSION NR: AP5021948

2

ties to the movement of domain walls. Curve 2 in Fig. 1 ($H = 325$ oersteds) characterizes only dislocation scattering. As can be seen, this increases with increasing degree of plastic deformation. Thus, as the degree of plastic deformation increases the proportions between the contributions of dislocation scattering and magnetoelastic scattering to the amplitude-dependent internal friction of the iron become reversed. As the temperature drops to -160°C , dislocation scattering decreases (Fig. 2); this is attributed to the increase in the resistance to the movement of dislocations with decreasing temperature. As can be seen from Fig. 2, the temperature dependence of dislocation scattering increases with increasing number of mobile dislocations as a result of the deformation. A possible explanation may be that, during the measurement of amplitude-dependent internal friction, the dislocations performing oscillatory motion with an amplitude of the order of $10^{-5}-10^{-4}$ encounter the temperature-dependent resistance of the crystal lattice. Orig. art. has: 4 figures.

ASSOCIATION: Institut metallofiziki (Institute of Metal Physics); TsNIIChermet im.
I. P. Bardina
SUBMITTED: 08Jun64

ENCL: 02

57

SUB CODE: MM, ME

NO REF Sov: 003

OTHER: 004

Card 2/4

L-1626-66

ACCESSION NR: AF5021948

ENCLOSURE: 01

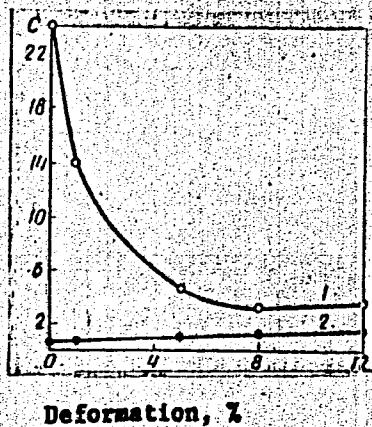


Fig. 1. Effect of degree of plastic deformation on amplitude dependence of internal friction of iron ($T = 20^\circ\text{C}$):

1 - $H = 0$; 2 - $H = 325 \text{ c.c.}$

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L 1626-66

ACCESSION NR: AF5021948

ENCLOSURE: 02

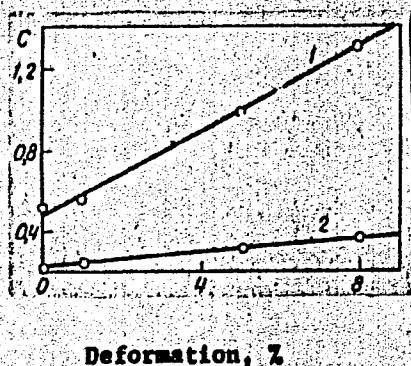


Fig. 2. Effect of degree of plastic deformation on the amplitude dependence of internal friction of iron ($H = 325$ oe):

1 - $T = 20^\circ\text{C}$; 2 - $T = -160^\circ\text{C}$

Card 4/4

BERESNEV, G.A. (Moskva); SARRAK, V.I. (Moskva); ENTIN, R.I. (Moskva)

Effect of temperature and interstitial impurities on energy
scattering during small shifting of dislocations in iron.
Izv. AN SSSR. Met. no.6:111-119 N-D '65. (MIRA 19:1)

1. Submitted February 12, 1965.

L 24328-66 EWT(m)/T/EWP(t) IJP(c) JD
ACC NR: AP6010425 SOURCE CODE: UR/0020/66/167/002/0322/032566

AUTHORS: Beresnev, G. A.; Sarrak, V. I.; Entin, R. I.

65
B

ORG: Central Scientific Research Institute of Ferrous Metallurgy im. I. P. Bardin (Tsentral'nyy nauchno-issledovatel'skiy institut chernoy metallurgii)

TITLE: Temperature dependence of the resistance of iron to deformation and the dislocation mobility

27

SOURCE: AN SSSR. Doklady, v. 167, no. 2, 1966, 322-325

TOPIC TAGS: iron, temperature dependence, crystal dislocation, crystal deformation, elastic stress, internal friction, crystal impurity, crystal lattice

ABSTRACT: To check on the causes of the strong temperature dependence of the elastic limit of metals with body-centered-cubic lattice, the authors have investigated the influence exerted on this elastic limit, taken as a function of the temperature, by the resistance of the crystal lattice itself to the motion of dislocations. The tests were

Card 1/2 UDC: 539.377

L 24328-66

ACC NR: AP6010425

made on commercial iron (0.025% C, 0.005% N) containing 0.33% Ti to bind the carbon and nitrogen into carbides and nitrides of titanium. The internal friction was measured at a frequency of approximately 1 cps. The amplitude dependent internal friction was measured at strains from 2×10^{-5} to 20×10^{-5} in a longitudinal constant magnetic field (325 Oe). Increasing the interstitial impurities from 10^{-7} to $10^{-3}\%$ greatly increases the resistance to deformation. The authors describe the effects produced by interstitial impurities, by the changes in density of the free dislocations participating in the deformation, and by the motion of the free dislocation. It is concluded from the results that the temperature dependence of the elastic limit of iron is essentially the consequence of an increase in the resistance of the crystal lattice to the motion of the free dislocations with decreasing temperature. The influence of the impurities and of the density of the free dislocations comes into play to the extent that they change the dislocation velocity, and the density of the moving dislocations or the multiplication of dislocations. This report was presented by Academician G. V. Kurdyumov. Orig. art. has: 4 figures and 2 formulas.

SUB CODE: 20, // SUBM DATE: 24 May 65 / ORIG REF: 004 / OTH REF: 005

Card

D2

2/2

ACC NR: AP7005135

SOURCE CODE: UR/0126/66/022/004/0606/0610

AUTHOR: Sarrik, V. I.; Shilov, N. A.

ORG: TsNIIChERMET

TITLE: The influence of cobalt on the tendency of iron toward brittle fracture

SOURCE: Fizika metallov i metallovedeniye, v. 22, no. 4, 1966, 606-610

TOPIC TAGS: iron base alloy, cobalt iron, brittleness, low temperature metal, transition temperature, tensile property, internal friction, activation energy

ABSTRACT: A study was done on the influence of cobalt on the brittle fracture of iron at low temperatures. The iron had the following compositions: 0.01-0.02% C, 0.20% Si, 0.17% Mn, 0.012% S, 0.0035% P, 0.013% O, 0.007% N, and 0.002% H. Impact testing was done at temperatures ranging from -192 to +100°C. The iron samples had a constant grain size of 35-40 μ and were alloyed with 5 and 10% Co. The impact strength, given as a function of temperature, showed that 5% Co lowered the transition temperature by 20°C, and 10% Co lowered it by 40°C. Tensile testing was done at temperatures ranging from +20 to -196°C at a constant crosshead speed of 2 mm/min. Tensile samples had a diameter of 10 mm and a gage length of 50 mm. The tensile strength and ductility were given as functions of temperature for pure and alloyed iron. The tensile transition temperature for pure iron was -100°C and -125°C for 5% Co. Five ten-

UDC: 539.4

Card 1/2

ACC NR: AP7005135

sile regions were separated on the basis of strength and ductility changes as a function of temperature. The mechanism by which cobalt improves the plasticity of iron at low temperatures was determined from internal friction properties on 0.8 mm samples which were vacuum-annealed to a constant grain size of 35-40 mm. A reverse pendulum was used to get the amplitude dependence of internal friction at temperatures ranging from 70 to 470°C. At low amplitudes (below about $4-15 \cdot 10^{-5}$ depending on temperature) the internal friction was independent of amplitude, while at higher amplitude it was proportional to amplitude. The slope in the amplitude dependent range was related to dislocation mobility or the energy for dislocation climb (ΔW). Values of $\lg \Delta W$ were given as a function of $1/T$ for the 10% Co alloy. Below 300°K, ΔW decreased as a result of increased lattice friction, while the sharp increase in ΔW above 500°K was caused by the locking of dislocations with interstitial impurities. The Cottrell relation for the concentration of impurities locking dislocations as an exponential function of temperature was given. Between 300 and 500°K, ΔW was not a function of temperature. The activation energies for dislocation interaction with impurity atoms (U_d) and the activation energies of mobile dislocations (U_r) were given for each alloy. Alloying with cobalt decreased both U_d and U_r , as well as the saturation temperature for impurity atoms. Thus cobalt had the same effect as nickel. Orig. art. has: 5 figures, 1 table, 3 formulas.

SUB CODE: 11/ SUBM DATE: 09Nov65/ ORIG REF: 009/ OTH REF: 001

Card 2/2

SARRAZIN, Olgierd

Annular pancreas. Polski przegl. chir. 32 no.11:1099-1102 '60.

l. Z III Kliniki Chirurgicznej A.M. w Poznaniu Kierownik: doc.
dr J. Borszewski.

(PANCREAS abnorm)

SARRAZIN, Olgierd

Anastomosis of a pancreatic cyst with the stomach in children.
Polski praecl. chir. 35 no.2:151-153 '63.

l. z III Kliniki Chirurgicznej AM w Poznaniu Kierownik: prof.
dr A. Piskorz.
(PANCREATIC CYST) (STOMACH)
(SURGERY OPERATIVE)
(ABDOMINAL INJURIES)

BULKIN, P.I.; SARRE, D.M.; YEMEL'YANOVA, N.I.; KRATYNSKIY, V.I.,
otv. red.; RUDAKOVA, N.I., tekhn. red.

[Official specifications and estimates for building, assembling, and repair work in 1960; estimates recalculated for the new price scale] Vedomstvennye normy i rastsenki na stroitel'nye, montazhnye i remontno-stroitel'nye raboty 1960 g.; rastsenki pereschitany iskhodia iz novogo masshtaba tsen. Moskva, Gosstroizdat. Collection V-48 [Building and assembling work using local materials in agriculture] Stroitel'nye i montazhnye raboty s primeneniem mestnykh materialov v sel'skom khozaiistve. 1961. 160 p. (MIRA 17:3)

1. Russia (1923- U.S.S.R.) Ministerstvo sel'skogo khozyaystva.

1. SARRE, M. F.
2. USSR (600)
4. Ensilage
7. Late fall sowing of sunflowers for silage.
Sots. zhiv. 11, No. 10, 1952.

9. Monthly List of Russian Accessions, Library of Congress, January 1953. Unclassified.

Sarre, M. F.

7752 Vidovoye rayonircvaniye silcsnykh, kormovykh, bakhchevykh kul'tur I
korneklutneplosov. utv. 21/x 1954 G.M., izd-vo m-va sel'skogo
khozyaystva sssr, 1955, 32S. 22sm. (glav. upr. s.-kh. propagandy
i nauchni m-va sel'skogo khozyaystva sssr). 20.000 ekz. Bespl.-V
kantse teksta avt. razrabotki: P.Ye. Marinich, A. I. Vytchikov,
M. P. Yelsukov, A. L. Mikhail'chuk, I. A. Polezhayev, M. F. Sarre,
M. N. Smirnov, B. F. Solov'yev. - (55-3885)

633.2/4;631.52

SC. Knizhnaya Letopis', Vol. 7, 1955

SARRE, M.F., agronom.

Late fall sowing of sunflowers for silage. Nauka i pered. op. v sel'-
khoz. 7 no.10:43-44 O '57. (MLRA 10:11)
(Sunflowers)

SARRE, M.F.

Sorghum is a valuable sugar plant. Sakh. prom. 32 no. 4:44-45 Ap
'58. (MIRA 11:6)

1.Gosufarstvennaya komissiya po sortoispytaniyu sel'skokhozyaystvennykh
kul'tur.

(Sorghum)

SARRE, M.F.

Make fuller and better use of Sudan grass by obtaining several harvests. Zhivotnovodstvo 23 no.6:70-72 Je '61. (MIRA 16:2)

1. Starshiy agronom Gosudarstvennoy komissii po sortoispytaniyu sel'skokhozyaystvennykh kul'tur.
(Sudan grass)

VISTELYUS, A. B., SARSADSKIEH, N. N.

Sanatoriums

Nature of change in the mineralogical composition of slime during successive washing of sands. Zap. Vses. mir ob. 81, No. 2, 1952

Monthly List of Russian Accessions, Library
Congress, September 1952, UNCLASSIFIED

"APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R001447220001-0

SARSADSKIKH, N.N.; POPUGAYEVA, L.A.

New data on the phenomenon of ultrabasic magmatism in the
Siberian Platform. Razved.i okh.nedr 21 no.5:11-20 8-0 '55.
(MLRA 9:12)

(Siberian Platform--Rocks, Igneous)

APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R001447220001-0"

SARSADSKIKH, N. N.: Master Geolog-Mineralog Sci (diss) -- "The mineralogy of friable and in situ rock of the eastern portion of the Siberian platform and the mineralogical criteria for prospecting for diamond deposits". Lenin-grad, 1959. 12 pp (Min Geology and Protection of Natural Resources USSR, All-Union Sci Res Geological Inst VSEGEI, Central Expedition), 150 copies (KL, No 11, 1959, 116)

SARSADSKIKH, N.N.; ROVSHA, V.S.

Genesis of mineral satellites of diamonds in Yakutian kimberlites.
Zap. Vses. min. ob-va 89 no.4:392-399 '60. (MIIFI 13:11)

1. Tsentral'naya ekspeditsiya Vsesoyuznogo nauchno-issledovatel'skogo geologicheskogo instituta, Leningrad.
(Yakutia--Kimberlites)

IL'INSKIY, G.A.; PLOTNIKOVA, M.I.; RAZUMIKHIN, N.V.; RYUMIN, A.K.; SARSADSKIH,
N.N.; SVARICHEVSKAYA, Z.A., doktor geogr. nauk; IL'INA, M.Ye., red.;
VODOLAGINA, S.D., tekhn. red.

[Fundamentals of placer deposit surveying] Osnovy poiskov rossyapei;
uchebnoe posobie. Leningrad, Izd-vo Leningr. univ., 1961. 122 p.
(MIRA 14:8)

1. Sotrudniki Leningradskogo gosudarstvennogo universiteta im. A.A.
Zhdanova (for Il'inskiy, Razumikhin, Ryumin, Svarichevskaya).
2. Sotрудники Всесоюзного геологического института (for Sarsadskikh,
Plotnikova)

(Ore deposits) (Geological survey)

BLAGUL'KINA, V.A.; ROVSHA, V.S.; SARSADSKIKH, N.N.

Mineralogy of kimberlite binder. Zap.Vses.min.ob-va 92 no.2:236-241
'62. (MIRA 15:6)

1. TSentral'naya ekspeditsiya Vsesoyuznogo nauchno-issledovatel'skogo
geologicheskogo instituta, Leningrad.
(Kimberlite) (Olivine)

ARTSYBASHEVA, T.F.; BLAGUL'KINA, V.A.; ROVSHA, V.S.; SARSADSKIKH, N.N.

Classification of kimberlites in Yakutia based on the kimber-
lites of the Alakit-Daldyn diamond-bearing region. Sov. geol.
6 no.1:70-81 Ja '63. (MIRA 16:6)

1. Vsescyuznyy nauchno-issledovatel'skiy geologicheskiy
institut.

(Yakutia—Kimberlite)

(Yakutia—Diamonds)

GALERKINA, S.G.; SARSADESKIKH, V.N.

Isolation of Triassic sediments on the eastern slope of the
Arctic Ural Mountains (southern Yamal Peninsula). Trudy
VNIGRI no.220. Geol. sbor. no.8:115-119 '63.
(MIRA 17:3)

SARSATSKIKH, P. I.

N/5
632
.83

Spravochnoye rukovodstvo po ozeleneniyu avtomobil'nykh dorog (Reference manual on the planting of greenery for automobile roads, by) P. I. Sarsatskikh i V. I. Obolenskiy. Moskva, Avtotransizdat, 1954.
188 p. illus., diagrs., tables.

ALEKSANDROV, Boris Sergeyevich; ALEKSEYEV, A.P.; ZABOLOTSKIY, F.D.;
KONDAKOV, A.Yu.; NEGODAYEV, V.I.; RYB'YEV, I.A.; SARSATSKIIH,
B.I.; CHAIUYSKIY, A.P.; SHOMINOV, I.S.; BABKOV, V.F., doktor tekhnicheskikh nauk, professor, redaktor; CHVANOV, V.G., redaktor; MAL'KOVA, N.V., tekhnicheskiy redaktor.

[Handbook for road foremen] Spravochnoe rukovodstvo dlja dorozhnogo mastera. Pod red. V.F.Babkova. Moskva, Nauchno-tekhn. izd-vo avto-transportnoi lit-ry, 1954. 450 p. [Microfilm] (MIRA 8:2)
(Roads)

SARSATSKIKH,P.I., uchenyy lesovod.

Special conditions of landscaping roads not taken into account
(Planting fruit trees along automobile highways." D.F. YUkhimchuk
Reviewed by P.I.Sarsatskikh) Avt.dor.18 no.5:30 S'55.

(MIRA 9:1)

(Roadside improvement) (Yukhimchuk,D.F.)

SARSATSKIKH, P.I.

PRYAKHIN, Viktor Dmitriyevich; SARSATSKIKH, P.I., redaktor; MAL'KOVA, N.V.,
tekhnicheskly redaktor

[Landscape automobile roads] Ozelenenie avtomobil'nykh dorog.
Moskva, Nauchno-tekhn.izd-vo avtotransp.lit-ry, 1957. 53 p.
(Roadside improvement) (MLRA 10:8)

SARSATSKIKH, Prokhor Ignat'yevich; GOLUBKOVA, Ye.S., red.; LAKHMAN, F.Ye.,
tekhn. red.

[Handbook for roadside landscaping] Spravochnoe rukovodstvo po
ozeleneniu avtomobil'nykh dorog. Izd.2., perer. Moskva, Nauchno-
tekhn. izd-vo avtotransp. lit-ry, 1958. 115 p.
(Roadside improvement)

IGOLKIN, Nikoley Ivanovich, inzh.; GAYDUK, Kirill Vasil'yevich, inzh.;
GUDIMA, Vladimir Savvich, inzh.; KORSUNSKIY, Mark Borisovich, kand.
tekhn.nauk; NIKONOV, Petr Vasil'yevich, inzh.; SARKIS'YANTS, Georgiy
Aleksandrovich, inzh.; SARSATSKIKH, Prokhor Ignat'yevich, inzh.;
ORNATSKIY, N.V., prof., doktor tekhn.nauk, glavnnyy red.; BYALO-
BZHEISKIY, G.V., kand.tekhn.nauk, red.; IVANOV, S.S., red.; GALAKTIO-
NOVA, Ye.N., tekhn.red.

[Manual for road builders; maintenance and repair of highways]
Spravochnik inzherera-dorozhnika; soderzhanie i remont avtomobil'nykh
dorog. Moskva, Nauchno-tekhn.izd-vo M-va avtomobil'nogo transporta
i shosseinykh dorog RSFSR, 1960. 326 p. (MIRA 13:9)
(Roads--Maintenance and repair)

SARSEKOV, A.S., Cand Geol Min Sci -- (diss) "Geomorphology
of the basin of the Mointy River." Alma-Ata, 1958,
14 pp (Acad Sci KSSR. Inst Geol Sci) 150 copies
(KL, 50-58, 121)

- 29 -

SARS~~K~~KOV, A.S.

Signs of recent tectonics in the Mointy Basin. Vest. AN Kazakh. SSR
14 no.3-74-77 Mr '58. (MIRA 11:5)
(Mointy Valley--Geology, Structural)

SABSEKOV, A.S.

Surface structure of the Mointy River basin and its principal stages
of development. Vest. AN Kazakh. SSR 14 no.4:67-72 Ap '58.
(Mointy Valley—Paleogeography) (MIRA 11:6)

KANLYBAYEVA, Zh.M.; ZHUKOVA, S.G.; KLINOVITSKIY, F.I.; SARSEMBAYEV, A.A.

Some results of using radioactive isotopes in observations of rock shifts in a layer of a massif. Trudy Inst.gor.dela AN Kazakh.SSR
9:40-57 '62. (MIRA 15:8)

(Radioisotopes—Industrial applications)
(Earth movements) (Coal mines and mining)

"APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R001447220001-0

VORONIN, I.S.; KERSHANSKIY, I.I.; TAKEZHANOV, S.T.; BEYLIN, Ya.Z.;
SARSEMBAYEV, A.S.; KAGARMANOV, O.Kh.

Introduction of the zinc condensation process in the electrothermal
treatment of silver foam. TSvet. met. 38 no.2:18-24 F '65.
(MIRA 18:3)

APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R001447220001-0"

SARSEMAYEV, M.M.

Characteristics of liver reaction to partial hepatectomy in
mice under the action of a carcinogenic amiroazo compound.
Vest. AMN SSSR 19 no. 11: 30-35. '64. (MIRA 18:3)

1. Institut eksperimental'noy i klinicheskoy onkologii AMN SSSR,
Moskva.

SARSEMBAYEV, M.S.; PONOMAREV, V.D.

Studying certain physicochemical properties of tellurium
trioxide. Vest.AN Kazakh.SSR 16 no.8:69-78 Ag '60.
(MIRA 13:9)

(Tellurium oxide)

5.2200

25172

S/031/60/000/011/005/008
A161/A133

AUTHORS: Sarsembayev, M.S., Ponomarev, V. D.

TITLE: On the viscosity and electric conductivity of the soda solutions of sodium tellurate

PERIODICAL: Akademiya nauk SSR, Vestnik, no. 11, 1960, 67 - 71

TEXT: No data of the viscosity and conductivity of soda solutions of sodium tellurate exist in literature, and the described investigation had a practical purpose - to obtain data for the electrolysis of tellurium. The initial material for the preparation of the solution was tellurium trioxide produced from tellurium oxide by a previously described method (Ref. 1) (Ponomarev and Sarsembayev, "Vestnik AN KazSSR", 1960, No. 8, 69); the soda content in the solution was kept constant, 143 g per liter, at changing tellurium contents. The viscosimeter used in the experiments had been described in (Ref. 2) (Usanovich, M.I., Sumarokova, T. N., and Udovenko, T. N. "Zhurnal fizicheskoy khimii", 1939, 9, 1967) and in (Ref. 3) (Sumarokova and Litvyak. "Izvestiya sektora platiny IONKh AN SSSR", 1952, v. 27, 127). The density of the electrolyte was measured by a picknometer graduated for water. The viscosity measurements were carried out at 20,
X

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X

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S/031/60/000/011/005/008
A161/A133

On the viscosity and electric conductivity ...

40 and 60°C, and the values for 30 and 50° obtained by calculations and curves. The viscosity of solutions differed considerably from the viscosity of water. Three curves are shown (Fig. 1) illustrating that the viscosity drops with rising temperature and the tellurium content in the solution has no effect. The formula used for calculations of viscosity is

$$\eta = \frac{\eta_B \cdot d_p \cdot \tau_p}{d_B \cdot \tau_B}$$

where η is the viscosity of the solution; d_p - the solution density; τ_p - time of the solution running; η_B , d_B , τ_B - the viscosity, density and running time of water at the same temperatures. The accuracy of measurements was within ± 0.0019 . The calculated viscosity factor (L) at different temperatures is given (Table 3):

No. of solution	L (-10^2) at temperatures, in °C			
	20 - 30	30 - 40	40 - 50	50 - 60
1	3.53	2.67	1.95	1.10
2	3.30	2.59	1.91	1.05
3	3.02	2.44	1.87	1.03

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A161/A133

On the viscosity and electric conductivity ...

Table 3 continued:

4.	2.84	2.35	1.83	0.96
5	2.69	2.28	1.77	0.93
6	2.59	2.28	1.72	0.89

(The tellurium content in the six test solutions was, in g/liter: No. 1 - 12.04; No. 2 - 6.02; No. 3 - 3.01; No. 4 - 1.505; No. 5 - 0.752; No. 6 - 0.376). The conductivity was measured with a P38 (R38) rheochord bridge and platinum plate electrodes coated by platinum black to reduce the polarization effect. The vessel constant was determined by the known method (by normal potassium chloride solution). The vessel was placed into a thermostat with a toluene regulator. The curve in figure 2 illustrates the results. The mean temperature factor of specific conductivity determined in the range of 20 - 60° was low, and indicating that the resistance of the solutions depended only little on the temperature. The equivalent conductivity of solutions calculated by variations of specific conductivity increased with rising temperature, but different results were obtained when the Yevstrop'yev's formula (Ref. 6) was used. As this has been stated by Ponomarey and Korostyshevskaya (Ref. 4) and K. S. Yevstrop'yev (Refs. 5,6), the mobility

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A161/A133

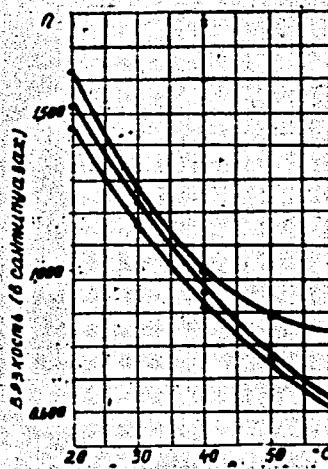
On the viscosity and electric conductivity ...

of ions drops with a rising viscosity, and the ratio of viscosity to conductivity at maximum dilution for aqueous and non-aqueous solutions at different temperatures is expressed by the formula $\eta \cdot A^n = \text{const}$ - where η - viscosity, A - equivalent conductivity, and n - a constant (Ref. 5). There are 2 figures, 6 tables and 6 Soviet-bloc references.

Figure 1:

The dependence of the viscosity of soda solutions of tellurate on the temperature (20 to 60°C); vertical legend: viscosity in centipoises.

Card 4/5



SARSENBAEV, R.; YESENOV, K.

Scientific syntax of the Kazakh language [in Kazakh]. Vest.AN
Kazakh SSR 18. no.3:90-92. Mr '62. (MIRA 15:3)
(Kazakh language—Syntax)

KANLYBAYEVA, Zh.M.; SARSENBAYEV, Ye.S.

Using the ultrasonic impulse method in studying the elastic properties of rocks from the Karaganda Basin. Trudy Inst. gor. dela AN Kazakh. SSSR 10:143-151 '63. (MIRA 16:8)

(Karaganda Basin—Rocks--Elastic properties)

GUMAROVA, F.G.; GOSTEVA, A.G.; TULEGENOV, Z.K.; MAKASHEVA, S.U.; POLOSUKHIN, A.P.; MUSABEKOV, A.M.; DANILOV, Yu.S.; NIGMATULIN, M.A.; ZAKHAROV, F.G.; LUZINA, Z.T.; NEPESOV, T.I.; STASYUNAS, I.P.; ISABEKOV, O.I.; SARSEMBALEVA, K.; KATSYURA, V.T.; LEVOVSKIY, A.S.; AKHMEDOV, K.Yu.; SUBKHANBERDIN, S.Kh.; KISLITSINA, N.P.; POLIKARPOV, S.V.; ZAIROV, K.S.; APSATAROV, A.A.; NOVOSEL'TSEV, V.N.; PETROV, N.N.; KHOMUTOV, M.V.; GALUSTYAN, A.S.; ARTYKOV, A.Ye.; DZHANDIL'DIN, N.D.; KOVRIGINA, M.D.; BEYSEBAYEV, M.; BUBLIK, V.N.; CHERNYSH, A.M.

Discussion on the report of S.R.Karynbaev, Minister of Public Health of the Kazakh S.S.R., on the status and improvement of medical care. Zdrav.Kazakh. 17 no.4/5 '57. (MIRA 12:6)

1. Zav. Alma-Atinskim oblastnym zdравотделом (for Gumarova).
2. Vrach bol'nitsy g.Leninogorska Vostochno-Kazakhstanskogo oblastzdravotdela (for Gosteva).
3. Zav. Karagandinskim oblastnym otdelom zdravookhraneniya (for Tulegenov).
4. Zav.Kzyl-Ordinskim oblastnym otdelom zdravookhraneniya (for Makasheva).
5. Vitse-prezident AN KazSSR (for Polosukhim).
6. Zav.Aktyubinskym oblastnym otdelom zdravookhraneniya (for Musabekov)
7. Ministr zdravookhraneniya Kirgizii (for Danilov).

(Continued on next card)

GUMAROVA, F.G.---(continued) Card 2.

8. Zav.Vostochno-Kazakhstanskim oblastnym otdelom zdravookhreniya (for Nigmatulin). 9. Chlen kollegii Ministerstva zdravookhraneniya SSSR (for Zakharov). 10. Zav.Kustanayskim oblastnym otdelom zdravookhraneniya (for Luzina). 11. Ministr zdravookhraneniya Turkmenskoy SSR (for Nepesov). 12. Zav.selskim vrachebnym uchastkom Priirtyshskogo rayona Pavlodarskoy oblasti (for Stasyunas). 13. Glavnnyy vrach Kapal'skuy rayonnoy hol'nitsy Taldy-Kurganskoy oblasti (for Isabekov). 14. Zav.zhenotdelom Yuzhno-Kazakhetanskogo obkoma partii (for Sarsenbayeva). 15. Zav. Dzhambulskim oblastnym otdelom zdravookhraneniya (for Katsyuha). 16. Glavnnyy vrach Alma-Atinskogo oblastnogo tuberkuleznogo dispansera (for Lenovskiy). 17. Ministr zdravookhraneniya Tadzhikskoy SSR (for Akhmedov). 18. Nachal'nik Kazaptekoupravleniya (for Subkhanberdin).

(Continued on next card)

GUMAROVA, F.G.----(continued) Card 3.

19. Zav. Semipalatinskym oblastnym otdelom zdravookhraneniya (for Kislitsina). 20. Predsedatel' respublikanskogo komiteta soyuza medraborotnikov (for Polikarpov). 21. Zam. ministra zdravookhraneniya Uzbekskoy SSR (for Zairov). 22. Zav. Alma-Atinskym gorodskim otdelom zdravookhraneniya (for Apsatarov). 23. Zav. Severo-Kazakhstanskim oblastnym otdelom zdravookhraneniya (for Novosel'tsev). 24. Zav. rayzdravotdelom Shortandin-skogo rayona Alkmolinskoy oblasti (for Petrov). 25. Zav. ministra zdravookhraneniya Soyusa SSR (for Khomitov). 26. Zav. ministra zdravookhraneniya ArmSSR (for Galustyan). 27. Predsedatel' Komiteta fizicheskoy kul'tury i sporta pri Sovete Ministrov KazSSR (for Artykov). 28. Sekretar' TSentral'nogo Komiteta Kommunisticheskoy partii Kazakhstana (for Dzhandil'din). 29. Ministr zdravookhraneniya Sovetskogo Soyusa (for Kovrigina). 30. Pervyy zamestitel' predsedatelya Soveta Ministrov KazSSR (for Beysebayev). 31. Uchastkovyy vrach Kustanayskoy oblasti (for Bublik). 32. Zam. predsedatelya Obshchestva Krasnogo Kresta Kazakhstana (for Chernysh).

(KAZAKHSTAN--PUBLIC HEALTH)

8/031/62/000/011/001/001
B104/B186

AUTHOR: Sarsembayeva, Kh. K.

TITLE: An investigation of the nature of coloring in optical calcite crystals with the help of absorption spectra

PERIODICAL: Akademiya nauk Kazakhskoy SSR. Vestnik, no. 11(212), 1962,
83 - 87

TEXT: The absorption spectra of 9 optical calcite crystals from various deposits in the Soviet Union are investigated with a CQ-4 (SF-4) spectrometer in the 220 to 1000 m μ . The light sources were a hydrogen lamp and an incandescent lamp. The samples were highly polished plates. Results: The absorption spectra of crystals from different sources vary. The spectra of samples of the same source are equal. The coloring of crystals from the same source was equal but differed in intensity (dim yellow, lemon-color, pink). Annealing at temperatures up to 400°C decreased the absorption power and decolorized the crystals. Irradiation with an X-ray tube having a tungsten plate (50 kv, 50 ma) increased the intensity of the

Card 1/2

An investigation of the nature ...

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B104/B186

natural color; which proved to be a function of the irradiation time. Annealed crystals decolorized much faster than others. Weak absorption maxima at $275 \text{ m}\mu$ and additional absorption at $475 \text{ m}\mu$ of irradiated crystals (the maxima of annealed and irradiated crystals are more distinct) apparently produce a pink coloring of the optical calcite. There are 3 figures.

Card 2/2

"APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R001447220001-0

PARASANOV, G.P.; SARSEMAYEVA, Kh.K.

Fluorescence properties of Iceland spar. Trudy Min.muz. no.13:
147-152 '62. (MIRA 16:2)
(Siberian Platform—Iceland spar)

APPROVED FOR RELEASE: 08/31/2001

CIA-RDP86-00513R001447220001-0"

KOLOMAKIN, G.; SARSEMOV, U.S.

Controlling paratyphoid fever in calves. Veterinariia 32 no.10:
46-47 O '55. (MIRA 8:12)

1. Director Taldy-Kurganskey oblastney vетеринарной laboratorii (for
Kolomakin). 2. Nachal'nik veterinarnogo otdela Taldy-Kurganskogo
oblastnogo upravleniya sel'skogo khozyaystva (for Sarsenov).
(COWS--DISEASES) (PARATYPHOID FEVER)

SOFIYEV, B.I.; SARSENOW, U.S.; KOLOMAKIN, G.A., kandidat veterinarnykh nauk;
STUDENTSOV, K.P.; VASKOVSKAYA, L.M.

Dry brucellosis vaccine from strain no. 19. Veterinariia 33 no.10:
40-44 O '56. (MLRA 9:10)

1. Machal'nik vetrupravleniya Ministerstva sel'skogo khozyaystva
Kazakhskoy SSR (for Sofiyev).
2. Nachal'nik veterinarnogo otdela Taldy-Kurganskogo oblastnogo
upravleniya sel'skogo khozyaystva (for Sarsenov).
3. Direktor ob'yektovetbaklaboratori (for Kolomakin).
4. Zaveduyushchiy brutselleznoy laboratoriye Kazakhskogo Nauchno-
issledovatel'skogo instituta (for Studentsov).
5. Glavnnyy veterinarnyy vrach Taldy-Kurganskogo rayona (for Vaskov-
skaya).

(Kazakhstan--Brucellosis in sheep--Preventive inoculation)

USSR/Diseases of Farm Animals. Diseases Caused by
Bacteria and Fungi.

R-1

Abs Jour: Ref Zhur-Biol., No 18, 1958, 83518

Author : Kolomakin, G. A., Sarsenov, U.S.

Inst : Institute of Veterinary Medicine, Kazakh Section of
the All-Union ordens Lenin Academy of Agricultural
Sciences imeni V. I. Lenin.

Title : Simultaneous Immunization of Cattle by Strain No
19 Brucella Vaccine and by Emcar Formolvaccine.

Orig Pub: Tr. In-ta vet. Kazakh. fil. VASKhNIK, 1957,
8, 79-81

Abstract: No abstract is given

Card 1/1

12

COUNTRY : USSR R
CATEGORY : Diseases of Farm Animals. Diseases Caused
by Helminths
ABS. JOUR. : RZhBiol., No. 6 1959, No. 26025
AUTHOR : Kolomakin, G. A.; Sarsenov, U. S.
INST. : Institute of Veterinary Medicine, Kuzakh Affiliates
TITLE : Certain New Data on the Employment of Phenothiazine-Salt Mixture in Helminthiases of Sheep
ORIG. PUB. : Tr. In-ta vet. Kuzakhsk. fil. VASKhNIL, 1957,
8, 438-442
ABSTRACT : The analysis of the results of experiments in
several years' standing use of phenothiazine-
salt mixture (1:9) on sheep in kolkhozes of
Taldy-Kurganskaya Oblast is given. It is noted
that liberal feeding of the above mixture has
*Institute of All-Union Academy of Agricultural
Sciences imeni Lenin

CARD:

1/2

44

USSR/Diseases of Farm Animals. Diseases caused
by Bacteria and Fungi R-2

Abs Jour: Ref Zhur - Biol., No 1, 1959, 2800

Abstract: which the cattle was vaccinated against
brucellosis, a diminution of organic re-
activity to the introduced antibrucella
vaccine did not take place in vaccina-
ted cattle.

Card 1/1

SARSER, Arkadiy Ionovich; KORDONSKIY, A.B., ovt. red.; SLAVOROSOV, A.Kh.,
red.izd-va; BOLDYREVA, Z.A., tekhn. red.; MINSKER, L.I., tekhn.
red.

[Surveying in mine building] Marksheiderskie raboty pri stroitel'-
stve shakht. Moskva, Gos.nauchno-tekhn.izd-vo lit-ry po gornomu
delu, 1961. 87 p. (MIRA 15:1)
(Mine surveying)

PIN'KOVSKIY, Gleb Stanislavovich; SARSER, A.I., retsenzent;
SLAVOROSOV, A.Kh., red.izd-va; ZHIVRHINA, G.V., tekhn.
red.; ROMANOVA, N.V., tekhn. red.

[Surveying operations during mine shaft sinking] Marksheider-
derskie raboty pri sooruzhenii shakhtnykh stvolov. Moskva,
Izd-vo "Nedra," 1964. 150 p. (MIRA 17:3)

SARSER, I.A.

Transistor voltage converter for radio transmitters. Sbor.luch.
rats.predl. pt. 2:69-71 '63. (MIRA 17:5)

1. Yakutskoye geologicheskoye upravleniye.

SARSÍKOVÁ, I. M.

CZECH

Hormones. The relation between physiological effect and chemical structure. I. M. Sarsíková (Med. KKL, Bratislava, Czech.) *Farmacia* 21, Suppl. 1-3(1952).—A review on N-contg. hormones with 17 references. II. *Ibid.* 22, Suppl. 1-7(1953).—A review on steroid hormones with 20 references. K. Macák

MAKSUMOV, S.S.; SARSIS'YANTS, S.L.; HEREMET'YEV, N.N.; CHICHERIN, P.I.;
ZAPROMETOVA, L.V.; ZHURAVLEV, N.A.

Virusological characteristics of the outbreak of poliomyelitis in
Tashkent in 1959. Vop. virus. 7 no.2:239 Mr-Ap '62. (MIRA 15:5)

1. Tashkentskiy nauchno-issledovatel'skiy institut vaktsin i syvorotok.
(TASHKENT--POLIOMYELITIS)

Loss of NOVA *111*

✓ 522. Compleximetric determination of bromoform in syrups. M. Šarfánová and Čížmancová (Dist. Control Lab., Bratislavská Medica, Czechoslovakia) (*Ceskosl. Farmac.*, 1955, 4 [4], 187-189).—The method consists in saponification of the bromoform and precipitation of the bromide thus formed with an excess of AgNO_3 soln. The AgBr is dissolved in an excess of aq. NH_3 soln. and $\text{K}_4\text{Ni}(\text{CN})_4$ is added. The Ag complexes with the cyanide and the liberated Ni is titrated with EDTA (disodium salt), with murexide as indicator. The method is suitable for the determination of bromoform alone or in syrups. The error is $< \pm 0.8$ per cent.

A. O. JAKUBOVIC

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CIA-RDP86-00513R001447220001-0"

M ✓ Rapid control method for the determination of alcohol
in tinctures Magda Šarťonová and Marek Štaksová
Krajská kontrolní ředitelství Mědiky Bratislava, Czechoslovakia 25 3.6.12.1966. A refractometer method for
rapid detn. of alc. in tinctures was developed. The refractive index of tinctures was measured at 20° with a refractometer and the Etalon 1000 refractometer. The formula
$$C = \frac{A - 1.33299}{B - 1.33299} \times 100$$
 where
$$A = n \text{ of the tincture, } d = d. \text{ of } H_2O \text{ at } 20^\circ (= 1.33299), c = d. \text{ of } H_2O \text{ at } 20^\circ (= 0.998229), \text{ and } C \text{ the vol.}\%$$

K. Macek